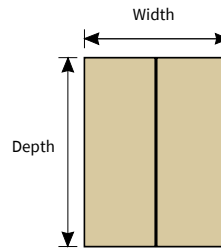


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	Calcs for <b>Mr Andrew Rose</b>	Date <b>18 May 2023</b>

## Timber Beam Design (BS 5268-2:2002)

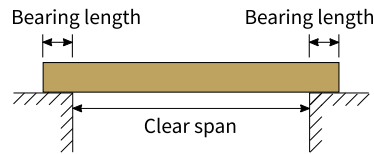
### Beam details

Beam	<b>94 x 200 mm (2 x 47x200 mm)</b>
	<b>C24 Grade Timber</b>
Timber strength class	<b>C24</b>
Service class of timber	<b>2</b>
Width	<b>b = 94 mm</b>
Depth	<b>h = 200 mm</b>



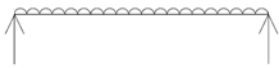
### Span details

Beam clear span	<b><math>L_{cl} = 2.95</math> m</b>
Bearing length	<b><math>L_b = 100</math> mm</b>
Beam effective span	<b><math>L_{eff} = L_{cl} + (2 \times (L_b / 2)) = 3.05</math> m</b>



Diagrams not to scale

### Loading details



#### Load 1: UDL - Timber floor (domestic dwelling)

Dead load  $F_{d,1} = 0.6 \text{ kN/m}^2 \times 1.5 \text{ m} = 0.9 \text{ kN/m}$

Imposed load  $F_{i,1} = 1.5 \text{ kN/m}^2 \times 1.5 \text{ m} = 2.25 \text{ kN/m}$

### Reactions (unfactored)

	Dead	Imposed	Total
Left reaction	<b>1.49 kN</b>	<b>3.43 kN</b>	<b>4.92 kN</b>
Right reaction	<b>1.49 kN</b>	<b>3.43 kN</b>	<b>4.92 kN</b>

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## Modification factors

Timber service class modification factor K2 as table 16

Bending parallel to grain	$K_{2,ben} = 1.00$
Compression perpendicular to grain	$K_{2,per} = 1.00$
Shear parallel to grain	$K_{2,shr} = 1.00$
Mean & min modulus of elasticity	$K_{2,mod} = 1.00$
Load duration factor	$K_3 = 1.00$
Bearing modification factor	$K_4 = 1.00$
Depth factor (BS5268-2 clause 2.10.6)	$K_7 = (300 / h)^{0.11} = 1.05$
Load sharing modification factor (BS5268-2 clause 2.10.11)	$K_8 = 1.10$
Modulus of elasticity modification factor (BS5268-2 clause 2.9)	$K_9 = 1.14$

## Modulus of elasticity

Timber minimum modulus of elasticity	$E_{min} = 7,200 \text{ N/mm}^2$
The minimum modulus of elasticity modified by the factor K9 should be used for deflections	$E = E_{min} \times K_{2,mod} \times K_9 = 8,210 \text{ N/mm}^2$

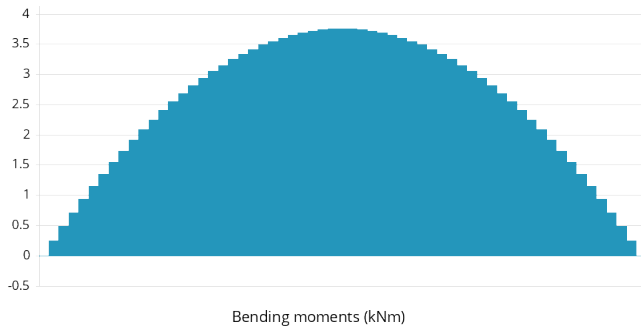
## Section properties

Area of section	$\text{Area} = b \times h = 18,800 \text{ mm}^2$
Inertia of timber about xx axis	$I_{xx} = b \times h^3 / 12 = 62,700,000 \text{ mm}^4$
Z to top edge of timber	$Z = b \times h^2 / 6 = 627,000 \text{ mm}^3$
Average density for C24 grade timber (BS 5268-2:2002 Table 8)	$\rho_{mean} = 420 \text{ kg/m}^3$
Self weight ( $g = 9.81 \text{ m/s}^2$ )	$F_{self} = b \times h \times L_{eff} \times \rho_{mean} \times g = 236 \text{ N}$

## Section design parameters

Design bending moment	$M_b = 3,750,000 \text{ Nmm}$
Design shear force	$F_{ve} = 4,920 \text{ N}$

## Check bending stress



Timber grade bending stress parallel to grain (BS5268-2 Table 8)

$$\sigma_{t,m,g,par} = 7.5 \text{ N/mm}^2$$

Permissible timber bending stress (factored)

$$\sigma_{t,m,adm} = \sigma_{t,m,g,par} \times K_{2,ben} \times K_3 \times K_7 \times K_8 = 8.63 \text{ N/mm}^2$$

Maximum bending moment

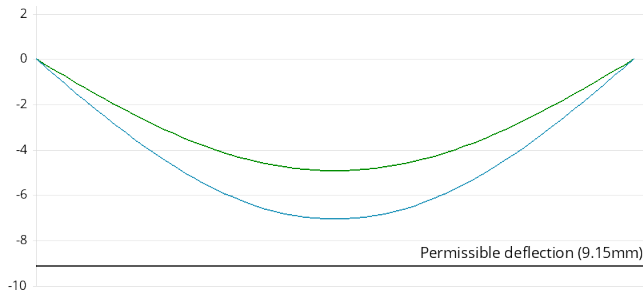
$$M = 3.75 \text{ kNm}$$

Applied bending stress in timber

$$\sigma_{t,m,max} = M / Z = 5.99 \text{ N/mm}^2$$

**Pass**  $\sigma_{t,m,max} \leq \sigma_{t,m,adm}$  (  $5.989 \text{ N/mm}^2 \leq 8.626 \text{ N/mm}^2$  ) applied bending stress in timber within permissible

### Check deflection (including shear deflection as required by clause 2.10.7)



Live load deflection (green) and total load deflection (blue) in mm

Deflection based on  $E = 8208 \text{ N/mm}^2$

Dead load deflection without shear

$$\delta_d = \mathbf{2.14 \text{ mm}}$$

Imposed load deflection without shear

$$\delta_i = \mathbf{4.93 \text{ mm}}$$

Total dead & imposed load deflection

$$\delta_t = \mathbf{7.07 \text{ mm}}$$

Modulus of rigidity

$$G = E / 16 = \mathbf{513 \text{ N/mm}^2}$$

Shape factor for rectangular section

$$K_F = \mathbf{1.2}$$

Shear area for beam

$$A_y = EA / K_F = \mathbf{15,700 \text{ mm}^2}$$

Total dead & imposed load

$$WT = \mathbf{9.84 \text{ kN}}$$

If total dead & imposed load applied as a UDL, additional deflection due to shear

$$\delta_{su} = WT \times L_{eff} \times 10^6 / (8 \times A_y \times G) = \mathbf{0.467 \text{ mm}}$$

Shear deflection

$$\delta_{shear} = \delta_{su} \times M / (WT \times L_{eff} / 8) = \mathbf{0.467 \text{ mm}}$$

Permissible deflection

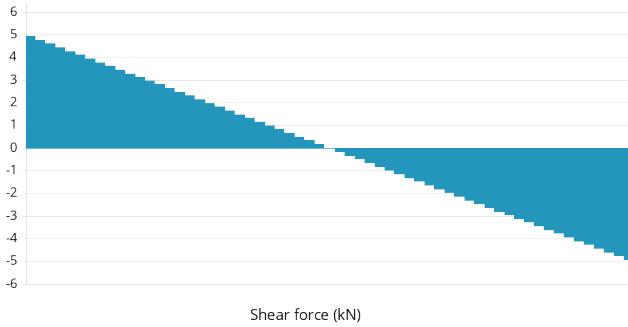
$$\delta_{adm} = 0.003 \times L_{eff} \times 10^3 \text{ (or max of 14mm)} = \mathbf{9.15 \text{ mm}}$$

Total deflection inclusive of shear

$$\delta_{max} = \delta_d + \delta_i + \delta_{shear} = \mathbf{7.54 \text{ mm}}$$

**Pass**  $\delta_{max} \leq \delta_{adm}$  (  $7.54 \text{ mm} \leq 9.15 \text{ mm}$  ), therefore OK for deflection

## Check shear stress



No notches to occur at the critical shear position.

Timber grade shear stress parallel to grain (BS5268-2 Table 8)

$$\tau_{t,g,par} = \mathbf{0.71 \text{ N/mm}^2}$$

Permissible shear parallel to grain (factored)

$$\tau_{t,adm} = \tau_{t,g,par} \times K_{2,shr} \times K_3 \times K_8 = \mathbf{0.781 \text{ N/mm}^2}$$

Permissible shear force on timber

$$F_{t,adm} = 2 \times \tau_{t,adm} \times b \times h / 3 = \mathbf{9,790 \text{ N}}$$

Design shear force

$$F_{ve} = \mathbf{4,920 \text{ N}}$$

**Pass**  $F_{ve} \leq F_{t,adm}$  (  $4922 \text{ N} \leq 9789 \text{ N}$  ) shear capacity of timber is greater than applied shear force, therefore OK

## Check bearing stress

Timber grade compressive stress perpendicular to grain (BS5268-2 Table 8)

$$\sigma_{t,c,g,\perp} = \mathbf{1.9 \text{ N/mm}^2}$$

Permissible compressive stress perpendicular to grain (factored)

$$\sigma_{t,c,adm} = \sigma_{t,c,g,\perp} \times K_{2,per} \times K_3 \times K_4 \times K_8 = \mathbf{2.09 \text{ N/mm}^2}$$

Timber bearing stress on support

$$\sigma_{t,c,max} = F_{ve} / (L_b \times b) = \mathbf{0.524 \text{ N/mm}^2}$$

**Pass**  $\sigma_{t,c,max} \leq \sigma_{t,c,adm}$  (  $0.524 \text{ N/mm}^2 \leq 2.09 \text{ N/mm}^2$  ) bearing stress is less than permissible timber stress, therefore OK

## Design summary

	Permissible	Applied/Actual	Utilisation	Result
Shear force (kN)	9.79	4.92	50.3 %	<b>OK</b>
Bending stress (N/mm <sup>2</sup> )	8.63	5.99	69.4 %	<b>OK</b>
Bearing stress (N/mm <sup>2</sup> )	2.09	0.52	25.1 %	<b>OK</b>
Deflection (mm)	9.15	7.54	82.4 %	<b>OK</b>

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## Notes

Joists to be bolted together with M12 bolts at 600mm spacings.

This design is in accordance with BS 5268-2:2002 Structural use of timber - Part 2: Code of practice for permissible stress design, materials and workmanship.

The depth to width ratio of the timber does not exceed 5 and as per the requirements of BS 5268-2 Table 19 there is no risk of buckling under design load provided; The ends are held in position and compression edge held in line, as by direct connection of sheathing, deck or joists.

Timber to be covered, this calculation is not to be used for timber which is fully exposed to the elements.

Wane as allowed in BS 4978:2007 + A2:2017 is permitted.